

# De Moivre's Theorem

$$e^{i\theta} = \cos\theta + i\sin\theta$$

$$e^x = 1 + x + \frac{1}{2!}x^2 + \frac{1}{3!}x^3 + \dots$$

$$e^{i\theta} = 1 + i\theta + \frac{1}{2!}(i\theta)^2 + \frac{1}{3!}(i\theta)^3 + \frac{1}{4!}(i\theta)^4 + \dots$$

$$\cos\theta = 1 - \frac{1}{2!}\theta^2 + \frac{1}{4!}\theta^4 \dots$$

$$i\sin\theta = i\left(\theta - \frac{1}{3!}\theta^3\right) \dots$$

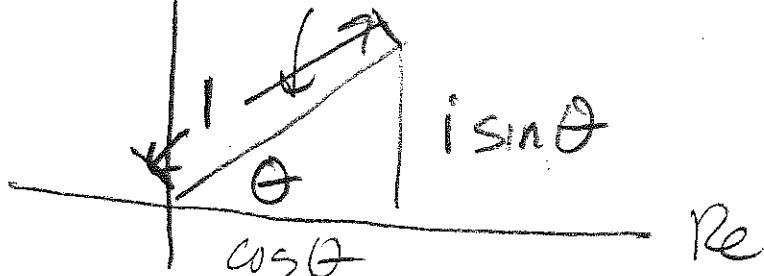
COMPARE ...

$$|e^{i\theta}| = \sqrt{(\cos\theta + i\sin\theta)(\cos\theta - i\sin\theta)}$$

$$= \sqrt{\cos^2\theta - i\cos\theta\sin\theta + i\sin\theta\cos\theta + \sin^2\theta}$$

$$= \sqrt{\cos^2\theta + \sin^2\theta} = 1 !$$

Plot ...  $\text{Im}$  /  $e^{i\theta}$



any number  $z \dots$

$$z = x + iy = \sqrt{x^2 + y^2} e^{i\theta} = re^{i\theta}$$

$$\theta = \tan^{-1}\left(\frac{y}{x}\right)$$

$$z^* = x - iy = \sqrt{x^2 + y^2} e^{-i\theta} = \overline{re^{i\theta}}$$

$$2 - 2i =$$

(A)  $2e^{i\pi/2}$

(B)  $2e^{-i\pi/4}$

(C)  $2e^{i\pi/4}$

(D)  $2e^{-i\pi/2}$

Complex Conjugate of  
 $e^{i\theta}$  when  $\theta$  is real

$$e^{i\theta} = \cos \theta + i \sin \theta$$

$$\begin{aligned}(e^{i\theta})^* &= (\cos \theta + i \sin \theta)^* \\&= \cos \theta - i \sin \theta \\&= e^{-i\theta}\end{aligned}$$

$$\begin{aligned}\text{so, } (e^{i\theta})(e^{i\theta})^* &= e^{i\theta} e^{-i\theta} \\&= e^{i(\theta-\theta)} = e^{i0} \\&= 1\end{aligned}$$

## Derivative of $e^{i\theta}$

$$\frac{d}{d\theta}(e^{i\theta}) = \frac{d}{d\theta}(\cos\theta + i\sin\theta)$$

$$e^{i\theta} \cdot i \stackrel{\text{check}}{=} -\sin\theta + i\cos\theta$$

$$(\cos\theta + i\sin\theta) \times i \stackrel{?}{=} -\sin\theta + i\cos\theta$$

$\downarrow$

$$i\cos\theta - \sin\theta \stackrel{?}{=} -\sin\theta + i\cos\theta \quad \checkmark$$

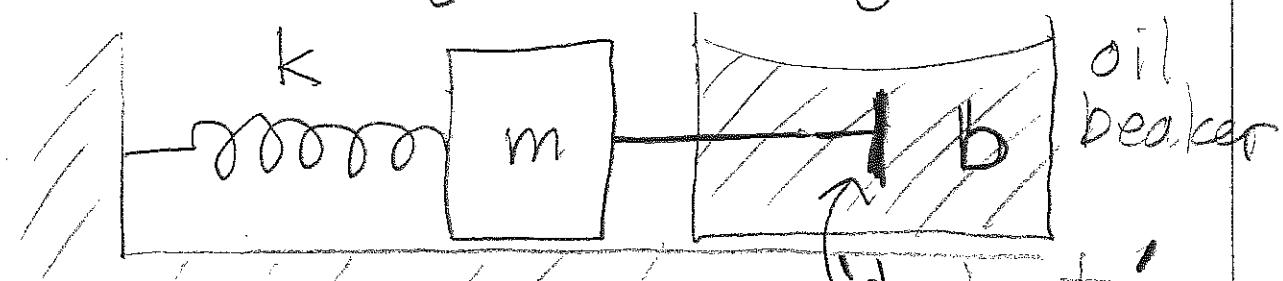
## Damped simple harmonic oscillator

model for many, many "damped" systems

→ car/bike shocks

→ musical instruments

→ electromagnetic wave generators



$b=0$  no damping       $b>0$  damping

$$m\ddot{x} = -kx$$

let  $x(t)$  satisfy  
above, &  $y(t)$  also

$$m\ddot{x} = -kx - b\dot{x}$$

-... opposes  
velocity.

satisfy it. Then  $z(t) = x(t) + iy(t)$ .  
 $z(t)$  is complex... use it to solve  
 $m\ddot{z} = -kz$ , and then use real part to  
describe actual motion. Arbitrary. Could take  $\text{Im}[z]$ .  
 $\frac{dx}{dt}$ .

Try  $z(t) = z_0 e^{\alpha t}$

$\alpha \rightarrow \text{complex}$   
**IMPORTANT**

$$\dot{z} = z_0 \alpha e^{\alpha t}$$

$$\ddot{z} = z_0 \alpha^2 e^{\alpha t}$$

$$m\ddot{z}/z_0 \alpha^2 e^{\alpha t} = -kz_0 e^{\alpha t}$$

$$\alpha^2 = -\frac{k}{m} = -\omega_0^2 \quad \text{"natural circular frequency"}$$

$$\alpha_{1,2} = \pm \sqrt{-\omega_0^2}$$

$$\alpha_{1,2} = \pm i\omega_0 \quad \boxed{\text{TWO SOLUTIONS}}$$

THIS CRUCIAL

GENERAL SOLUTION

WILL PERSIST

$$z(t) = z_A e^{\alpha_1 t} + z_B e^{\alpha_2 t}$$

$$= z_A e^{i\omega_0 t} + z_B e^{-i\omega_0 t}$$

want real part, means

$$z_A = \frac{1}{2} X_m e^{i\phi}$$

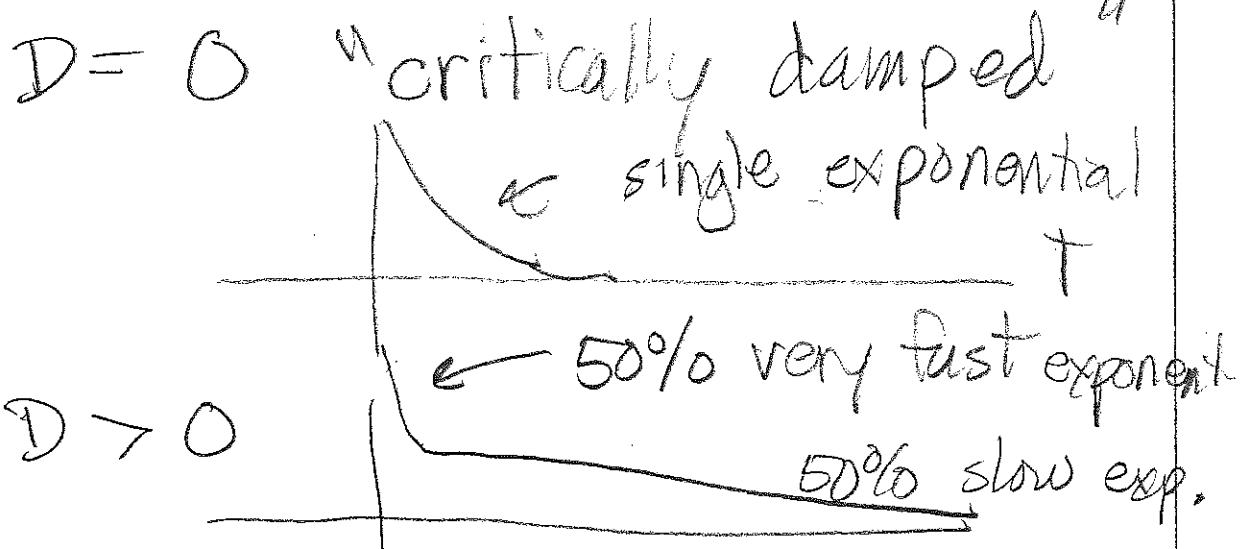
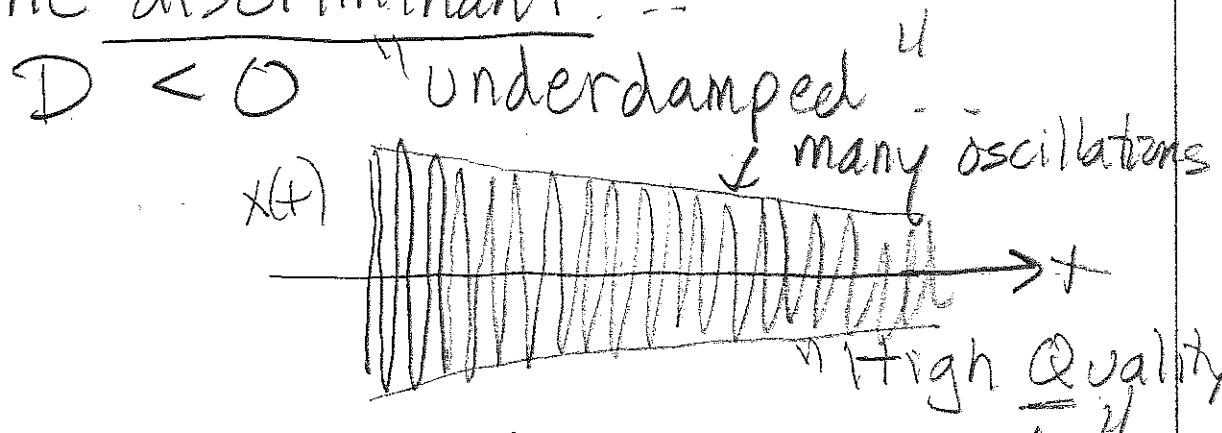
$$z_B = \frac{1}{2} X_m e^{-i\phi}$$

has all the info ... no loss of generality  
 and  $z(t) = \frac{1}{2} x_m (e^{i\omega t + i\phi} + e^{-i\omega t - i\phi})$   
 $= x_m \cos(\omega t + \phi)$

Now make  $b \neq 0$ ,  $b > 0$  "DAMPING"

Important: frequencies in  
 exponent now solutions to  
 the quadratic equation (12 year-olds,  
 sing solutn!)

Physical character will depend  
 on the discriminant. --



We'll focus on underdamped...  
a little on critically damped.

$$m\ddot{z} = -kz - b\dot{z} \quad z = z_0 e^{\lambda t}$$

$$mz_0^2 e^{\lambda t} = -kz_0 e^{\lambda t} - bz_0 \lambda e^{\lambda t}$$

$$m\lambda^2 = -k - b\lambda \quad \leftarrow \text{divide through by } m, \text{ rearrange}$$

$$\lambda^2 + \frac{b}{m}\lambda + \frac{k}{m} = 0$$

call  $\gamma$  (damping)  $\omega_0^2$ , dimensions / time<sup>2</sup>

$\gamma \rightarrow 0$  no damping.

THE

QUADRATIC.

$$\lambda^2 + \gamma\lambda + \omega_0^2 = 0$$

$$\Delta = " \sqrt{b^2 - 4ac} " = 2 \sqrt{\left(\frac{b}{2}\right)^2 - ac}$$

$$= 2 \sqrt{\left(\frac{\gamma}{2}\right)^2 - \omega_0^2} \quad \begin{array}{l} \text{LOOK! } \gamma \rightarrow 0 \\ = 2i\omega_0 \end{array}$$

UNDERDAMPED  $\left(\frac{\gamma}{2}\right)^2 - \omega_0^2 < 0$

CRITICALLY DAMPED  $\left(\frac{\gamma}{2}\right)^2 - \omega_0^2 = 0$

OVERDAMPED  $\left(\frac{\gamma}{2}\right)^2 - \omega_0^2 > 0$

solution

→ pretty similar to  $x_m \cos(\omega_0 t + \phi)$

$$\omega_{1,2} = \frac{-\gamma \pm \sqrt{\left(\frac{\gamma}{2}\right)^2 - \omega_0^2}}{2}$$

definition

$$= -\frac{\gamma}{2} \pm \sqrt{\left(\frac{\gamma}{2}\right)^2 - \omega_0^2} \quad -\omega_1^2 \equiv \left(\frac{\gamma}{2}\right)^2 - \omega_0^2$$

$$x(t) = \frac{1}{2} x_m \left[ e^{\frac{-\gamma t}{2}} e^{i w_1 t + i \phi} + e^{\frac{-\gamma t}{2}} e^{-i w_1 t - i \phi} \right]$$

COMMON!

$$x(t) = x_m e^{\frac{-\gamma t}{2}} \cos(w_1 t + \phi) \quad \text{REAL}$$

Principal Physical Effect -  $e^{\frac{-\gamma t}{2}}$

Secondary:  $\omega_1 \neq \omega_0$ , but shift is  $w_1$  second order!!

$x_m, \phi \rightarrow$  initial conditions

- release from rest,  $\phi=0$ ,

$x_m$  = initial displacement

Energy

$$= \frac{1}{2} k x^2(t) + \frac{1}{2} m \dot{x}^2(t)$$

$$\dot{x}(t) = x_m \left[ -\frac{\gamma}{2} e^{-\frac{\gamma t}{2}} \overset{\approx w_0}{\cos(w_1 t + \phi)} - w_1 e^{-\frac{\gamma t}{2}} \overset{\approx w_0}{\sin(w_1 t + \phi)} \right]$$

if  $\gamma \gg 0$ , neglect  $\approx w_0 \approx w_1$

$$\ddot{x}(t) \approx -x_m w_0 e^{-\gamma t/2} \sin(w_0 t + \phi)$$

$$E = \frac{1}{2} k x_m^2 e^{-\gamma t} \cos^2(w_0 t + \phi) + \frac{1}{2} m x_m^2 w_0^2 e^{-\gamma t} \sin^2(w_0 t + \phi)$$

$\approx w_0$        $m w_0^2 = k$

$$= \frac{1}{2} k x_m^2 e^{-\gamma t} (\underbrace{\cos^2(w_0 t + \phi) + \sin^2(w_0 t + \phi)}_{=1})$$

$$E \approx \frac{1}{2} k x_m^2 e^{-\gamma t}$$

PURELY  
EXPONENTIALLY  
DECAYS

at max      gets square to  $\gamma$

Quality Factor Q      Fractional energy loss/radian

$\equiv 1/Q$  (dimensionless).

$$Q = \frac{E}{-\Delta E} = \frac{\frac{1}{2} k x_m^2 e^{-\gamma t}}{\left(\frac{1}{2} k x_m^2 \gamma e^{-\gamma t}\right)}$$

$$Q = \frac{w_0}{\gamma} \quad \text{DIMENSIONLESS}$$

$Q \rightarrow \infty$  then  $\gamma \rightarrow 0$ . NO DAMPING

"high quality"

## Intuition on Q... (cuto do deriv!)

Lots of Systems use Q  
as a measure of "Quality"  
= absence of damping.

- ① Watch until peak amplitude falls to  $\approx e^{-\pi} \approx 4\% = \frac{1}{23}$  of original (LOTS of cycles.)
- ② Count  $\nu$ , # cycles.  $\boxed{Q = \nu!}$

$$\gamma = \frac{\omega_0 +}{2\pi} \approx \frac{\omega_0 +}{2\pi}$$

$$so \quad + = \frac{2\pi\nu}{\omega_0}$$

$$e^{-\frac{\gamma+}{2}} = e^{-\pi}$$

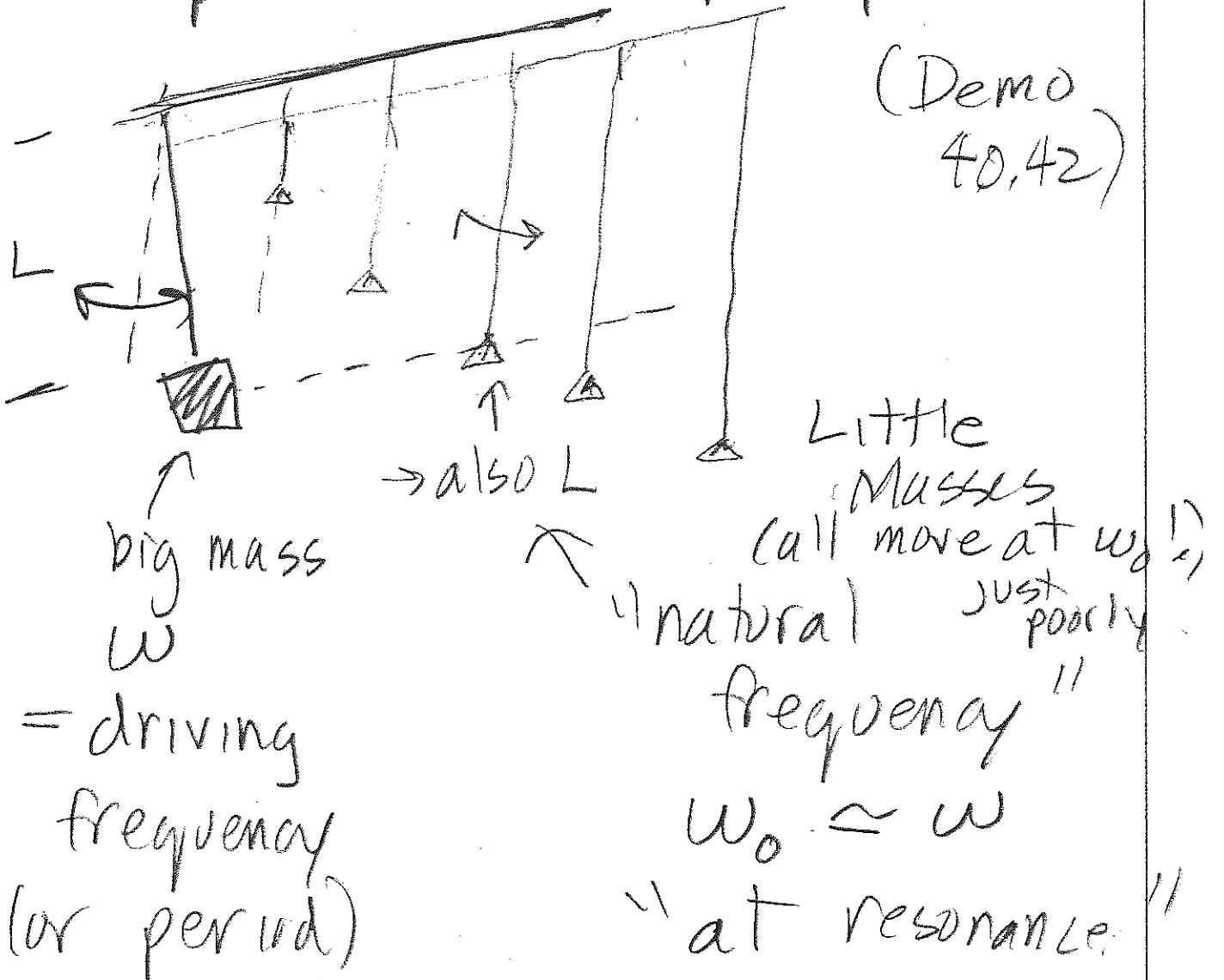
$$so \quad \gamma \cdot \frac{2\pi\nu}{2\omega_0} = \pi$$

$$\boxed{\nu = \frac{\omega_0}{\gamma} = Q}$$

# Forced, Damped Oscillator.

$\omega \rightarrow$  driving circular frequency

Example was multiple pendula.



= driving  
frequency  
(or period)

$$\omega = \sqrt{\frac{g}{L}}$$

$\rightarrow$  phase shifted by  $-i$   
 $\rightarrow$  biggest amplitude.

Generally --

$$m \ddot{x} = -kx - b\dot{x} + F_0 \cos(\omega t)$$

driving      spring      damping      driver  
 behavior      or driven      system  
 $F_0 e^{i\omega t} = \cos(\omega t)$

$$x = \operatorname{Re}(z) \text{ as before}$$

then  $\ddot{z} = -\frac{k}{m} z - \frac{b}{m} \dot{z} + \frac{F_0}{m} e^{i\omega t}$

$\underline{\text{natural freq}} \quad \underline{\dot{z}}$   
 $= -\omega_0^2 z - \gamma \dot{z} + \frac{F_0}{m} e^{i\omega t}$

IN STEADY STATE  $\rightarrow$  large times

$$z = z_0 e^{i\omega t}$$

$$\dot{z} = i\omega z_0 e^{i\omega t}$$

cancels everywhere.

$$\ddot{z} = -\omega_0^2 z_0 e^{i\omega t}$$

$$-\omega_0^2 z_0 e^{i\omega t} = -\omega_0^2 z_0 e^{i\omega t} - i\gamma \omega_0 z_0 e^{i\omega t} + \frac{F_0}{m} e^{i\omega t}$$

This time,  $Z_0$  doesn't cancel,  
but

$$Z_0(w_0^2 - w^2 + i\gamma w) = \frac{F_0}{m}$$

$$Z_0 = \frac{F_0}{m(w_0^2 - w^2 + i\gamma w)}$$

$$= \frac{F_0}{m w_0^2 \left( 1 - \left(\frac{w}{w_0}\right)^2 + i \frac{\gamma w}{w_0^2} \right)}$$

$$m \cdot \frac{k}{m} = k \quad \text{dimensionless}$$

$$Z_0 = \frac{F_0}{k} \cdot \frac{1}{\left[ 1 - \left(\frac{w}{w_0}\right)^2 + i \frac{\gamma w}{w_0^2} \right]}$$

DISPLACEMENT

CAUSED BY

$F_0$  IF STATIC

Resonant Factor  
Imagine this as  
a factor of  $w$

$$\text{then } X(t) = \frac{F_0}{k} \operatorname{Re} \left[ \frac{1}{1 - \left(\frac{w}{w_0}\right)^2 + i \frac{\gamma w}{w_0^2}} e^{i\omega t} \right]$$

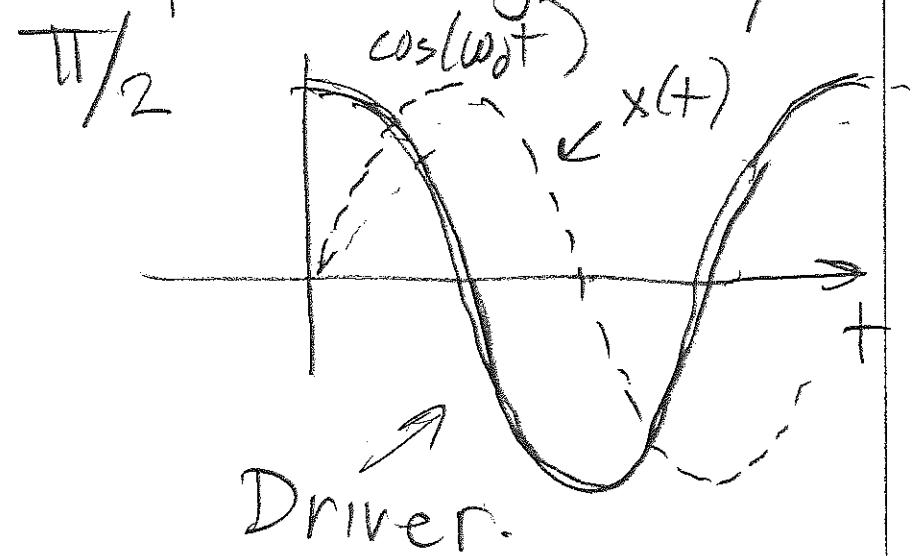
(A)  $\omega = \omega_0$  RESONANCE

$$x(t) = \frac{F_0}{K} \operatorname{Re} \left[ -i \frac{\omega_0}{\gamma} e^{i\omega_0 t} \right]$$

↗ STEADY STATE      THE - P

$$= \underbrace{\frac{F_0}{M} Q}_{\text{M}} \sin(\omega_0 t)$$

- DRIVE WITH  $\cos(\omega_0 t)$
- Response ↑ by factor of  $Q$  = Quality.
- Response Lags by  $\pi/2$



Driver:

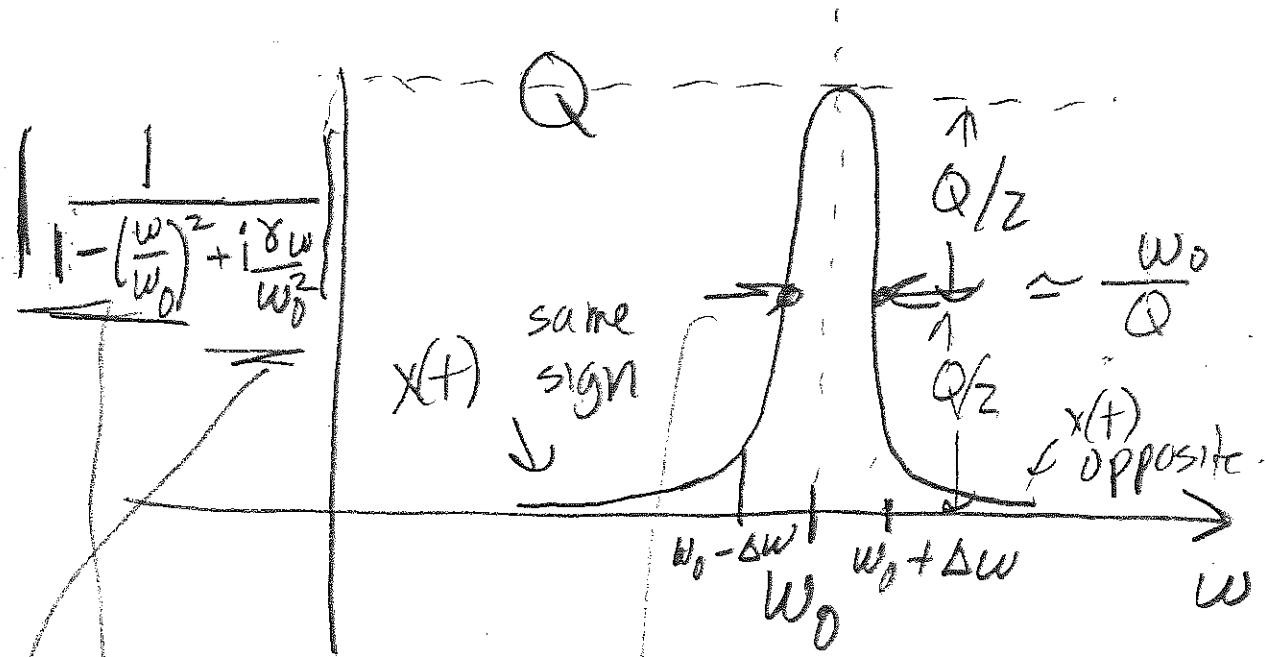
(B)  $\omega < \omega_0$   $x(t) + F_0 \omega s(\omega t)$   
SAME SIGN,  $x(t)$  small

(C)

$$\omega > \omega_0 \quad x(t) + F_0 \cos(\omega t)$$

OPPOSITE SIGN.

"Resonance Curve"



"Width"  $\rightarrow$  FWHM  $\approx \frac{w_0}{Q}$   
Full Width Half Max

$$1 - \left( \frac{\omega_0 \pm \Delta\omega}{\omega_0} \right)^2 \approx 1 - 1 \mp 2 \frac{\omega_0 \Delta\omega}{\omega_0^2} + \frac{\Delta\omega^2}{\omega_0^2}$$

$$\approx \mp 2 \frac{\Delta\omega}{\omega_0}$$

$$\frac{\Delta\omega}{\omega_0^2} \approx \frac{\Delta\omega}{\omega_0} = \frac{1}{Q} \quad \omega = \omega_0 \pm \Delta\omega$$

$$\left| \frac{1}{1 \mp 2 \frac{\Delta\omega}{\omega_0} + \frac{i}{Q}} \right| = \sqrt{1 + \left( \frac{\Delta\omega}{\omega_0} \right)^2 + \left( \frac{1}{Q} \right)^2} = \frac{Q}{2}$$

$$4 \left( \frac{\Delta\omega}{\omega_0} \right)^2 + \frac{1}{Q^2} = \frac{4}{Q^2}$$

$$\frac{\Delta\omega}{\omega_0} = \sqrt{\frac{3}{4}} \frac{1}{Q}$$

$$\boxed{\Delta\omega = \sqrt{\frac{3}{4}} \frac{\omega_0}{Q}} \approx \frac{\omega_0}{Q}$$

Key point: to see maximum resonant effect, must tune  $\omega$  to within  $\sim Y_Q$  of  $\omega_0$  (%-wise).

Disclaimer: for energy,  
not amplitude,

$$\Delta\omega = \frac{\omega_0}{Q} \quad ---$$

$\sqrt{\frac{3}{4}}$  comes from  
amplitude.